

HEARING AID WITH DIGITAL COMPRESSION RECAPTURE

Cross-Reference to Related Application(s)

This patent application is a continuation of PCT Application
5 No. PCT/US01/46476, filed on December 5, 2001, entitled "Hearing Aid Digital Automatic Gain Control," which is a continuation-in-part of U.S. Patent Application No. 09/730,200 filed on December 5, 2000, entitled "Digital Automatic Gain Control," the specifications of which are hereby incorporated by reference.

10 Technical Field

The present invention relates generally to audio signal processing. More particularly, it pertains to inhibiting distortions that arise from adjusting gains of preamplifiers and preserving signal compression information for subsequent processing, especially in hearing aids.

15 Background

Sound systems can be broken down into three general components: an input device, such as a microphone; a processing system; and an output device, such as a speaker. Sounds are picked up by the microphone, transmitted to the processing system
20 where they are processed, and then projected by the speaker so that the sounds can be heard at an appropriate distance. Both the microphone and the speaker are generally considered to be transducers. One application of the sound system is a hearing aid.

A transducer is a device that transforms one form of energy into another form of energy. In the case of a microphone, sound energy, which can be detected by the
25 human ear in the range of 20 Hertz to 20,000 Hertz, is transformed into electrical energy in the form of an electrical signal. The electrical signal can then be processed by a processing system. After the signal is processed, the speaker transforms the electrical energy in the electrical signal to sound energy again.

Before reaching the processing system, the electrical signal is amplified by a
30 preamplifier using a certain gain. However, if the electrical signal already represents a

powerful sound energy, the amplified electrical signal may be at a level beyond the linear operating range of the signal processing circuitry following the preamplifier. To limit the electrical signal to the operating range of the signal processing circuitry, an automatic gain control is used.

5 The automatic gain control detects the level of the waveform of the electrical signal, compares the level to a threshold, and adjusts the gain of the preamplifier to decrease the level of the electrical signal if the envelope is higher than the threshold. When the level is below the threshold, the automatic gain control increases the gain to its uncompressed level.

10 However, the automatic gain control, which is supposed to help, also hinders by adding undesired distortions to the electrical signal. These undesired distortions are frustrating to users of sound systems in general, but are particularly debilitating for users of hearing aids since these users depend upon such aids to maintain their ability to communicate. Without an acceptable solution to the undesired distortions, the optimum
15 level of performance desired by the end user will not be achieved.

 Thus, what are needed are systems, devices, and methods to inhibit AGC-induced distortions in sound systems, such as hearing aids.

 Automatic gain control may further frustrate users of sound systems by compressing the input signal to prevent overload of circuit elements such as analog to
20 digital converters. Compressing a signal means reducing the amplitude of the signal so that the signal remains below a threshold. The application of the gain to reduce the signal amplitude is typically non-linearly applied. Thus, the automatic gain control introduces distortion into the signal. Distorting the amplitude of the signal may also distort the information contained in the compressed portion of the input signal. This is
25 particularly undesirable of users of hearing aids. It is believed that some of the information contained in a hearing aid input signal may be contained in the compressed portion of the input signal. A hearing aid wearer would not receive the information in the compressed portion of the input signal. Obviously, such a loss would be detrimental to a hearing aid wearer.

Thus, what are further needed are systems, devices, and methods to recover AGC-induced distortions while storing the information contained in the original input signal that is lost due to compression in sound systems, such as hearing aids. More particularly, what is needed is a system to reverse the effects of non-linear application
5 of the gain during compression to thereby reconstruct the original signal.

Summary

The above-mentioned problems with distortions in audio signal processing as well as other problems are addressed by the present invention and will be understood by
10 reading and studying the following specification. Systems, devices, and methods are described which inhibit AGC-induced distortions. Moreover, systems, devices and methods are described which return compressed signals to essentially their original amplitudes.

One illustrative embodiment includes a method for providing automatic gain
15 control. The method includes smoothing an envelope of an input signal having a gain and adjusting the gain that is applied to the input signal. The act of adjusting is dependent on the level of the envelope relative to a threshold. The act of smoothing inhibits distortions arising from apparent modulation of the input signal.

Another illustrative embodiment includes a hearing aid. The hearing aid
20 includes an analog part for detecting sound and a digital part for processing the sound. The hearing aid further includes an adjuster to adjust the gain so as to amplify an input signal, and a detector to form a smooth envelope that is a rectified version from the input signal. The detector presents the smooth envelope to the adjuster. The adjuster adjusts the gain that is applied to the input signal. The adjuster adjusts the gain based
25 on the level of the envelope relative to a threshold.

The digital system as will be described has a number of benefits not seen before. One benefit is an enhanced manufacturing process that reduces a need for external components, such as capacitors, and the need to couple the external components to a circuit through I/O pins. Another benefit includes a reduction in the die area required to
30 implement the digital automatic gain control loop. Other benefits include an enhanced

control of the tolerance of the bandwidth of the automatic gain control, and the tolerance of the loop time constants of the automatic gain control. The system also benefits from an enhanced power efficiency and low operating voltage performance. Additionally, the system allows a non-linear signal processing by selectively controlling the gain of the preamplifier or providing information to a Nyquist-rate digital signal processor to compensate for adaptive gain changes in the preamplifier.

An embodiment of a sound system includes means for keeping information relating to a compressed portion of an input signal. In an embodiment, the means for keeping information includes a circuit which supplies a variable gain control signal to a digital signal processor. In an embodiment, the circuit supplies a mathematical inverse of the variable gain control to the digital signal processor. The digital signal processor then, if desired, digitally reconstructs the signal to include the compressed portion. An embodiment of circuit processes the variable gain control signal to supply a transfer signal to be combined with the compressed input signal to thereby recreate the input signal. Accordingly, the compressed portions of the signal are added back into the signal output from the input stage of a hearing aid. In an embodiment, the compressed input signal and transfer signal are digital signals and digitally combined to reconstruct the input signal to include the compressed portion in an embodiment, the transfer signal includes the inverse of the digital variable gain control signal. In an embodiment, the inverse of the variable gain control signal is also a gain signal that is applied to the compressed signal to essentially reconstruct the original signal.

These and other embodiments, aspects, advantages, and features of the present invention will be set forth in part in the description which follows, and in part will become apparent to those skilled in the art by reference to the following description of the invention and drawings or by practice of the invention. The aspects, advantages, and features of the invention are realized and attained by means of the instrumentalities, procedures, and combinations particularly pointed out in the appended claims.

Brief Description of the Drawings

Figure 1 is a block diagram of a system according to one embodiment of the invention.

Figure 2 is a graph of a signal according to one embodiment of the invention.

5 Figure 3 is a graph of a signal according to one embodiment of the invention.

Figure 4 is a graph of a signal according to one embodiment of the invention.

Figure 5 is a graph of a signal according to one embodiment of the invention.

Figure 6 is a block diagram of a system according to one embodiment of the invention.

10 Figure 7 is a block diagram of a filter according to one embodiment of the invention.

Figure 8 is a block diagram of a filter according to one embodiment of the invention.

15 Figure 9 is a process diagram of a method according to one embodiment of the invention.

Figure 10 is a block diagram of a system according to one embodiment of the invention.

Figure 11 is a graph of a signal according to one embodiment of the invention.

Figure 12 is a graph of a signal according to one embodiment of the invention.

20 Figure 13 is a graph of a signal according to one embodiment of the invention.

Figure 14 is a graph of a signal according to one embodiment of the invention.

Figure 15 is a graph of a signal according to one embodiment of the invention.

Detailed Description

In the following detailed description of the invention, reference is made to the accompanying drawings that form a part hereof, and in which are shown, by way of illustration, specific embodiments in which the invention may be practiced. In the drawings, like numerals describe substantially similar components throughout the several views. These embodiments are described in sufficient detail to enable those skilled in the art to practice the invention. Other embodiments may be utilized and structural, logical, and electrical changes may be made without departing from the scope of the present invention.

The embodiments of the invention focus on inhibiting distortions that arise from automatic adjustments of the gain of preamplifiers in sound systems. An ear-worn hearing aid is an example of such a sound system. As discussed hereinbefore, the automatic gain control, which helps in adjusting the gain of the preamplifier, also hinders by adding undesired distortions to the electrical signal.

The automatic gain control detects the envelope of the waveform of the electrical signal, compares the envelope to a threshold, and adjusts the gain of the preamplifier. The act of detecting the envelope includes sampling the waveform of the electrical signal to form samples of the envelope that are representative of the magnitude of the waveform. Each sample of the envelope is then compared to the threshold by the act of comparing. If any of the samples is greater than or less than the threshold, the gain of the preamplifier is adjusted by the act of adjusting. After the gain is adjusted, the preamplifier amplifies the electrical signal so as to form an amplified electrical signal.

A curious phenomenon may occur during the acts of detecting, comparing, and adjusting. The magnitude of the waveform of the amplified electrical signal, for certain frequencies, appears as if it has been modulated so as to form an amplitude modulation. This amplitude modulation is unwanted because it will give rise to the undesired distortions. This phenomenon occurs when the frequency of the electrical signal is slightly removed from a rational factor of the sampling frequency.

Each sample of the envelope that includes the apparent modulation is then compared to the threshold by the act of comparing. If any of the samples is greater than

or less than the threshold, the gain of the preamplifier is adjusted by the act of adjusting. However, because of the apparent modulation in the envelope, the gain no longer tracks the true envelope of the signal but varies periodically. This gain, which varies periodically, is applied to the electrical signal by the preamplifier. The preamplifier produces an amplitude modulation as a result of the application of the gain, which varies, to the electrical signal.

This amplitude modulation adds undesired frequency components to the electrical signal. These undesired frequency components are distortions which are inhibited by the embodiments of the invention. The embodiments of the invention solve this and other problems as discussed hereinbelow.

Figure 1 is a block diagram of a system in accordance with one embodiment. A system 100 includes a microphone 102. The microphone 102 transduces sound energy into an electrical signal. The microphone 102 is powered by a voltage supply 104. The microphone 102 also couples to ground 106.

The electrical signal is presented to a capacitor 108. The capacitor 108 removes the direct-current (DC) component of the electrical signal and presents the electrical signal to a preamplifier 110 without the direct-current component. The preamplifier 110 amplifies the electrical signal using a gain. As discussed herein, the electrical signal may be at a level that is too weak for subsequent circuitry to process. The preamplifier 110 adjusts the level of the electrical signal so that the electrical signal is within a range that is appropriate for further processing.

The electrical signal, which has been amplified, is presented to an analog-to-digital converter 112. The analog-to-digital converter 112 converts the electrical signal from an analog form to a digital form. The digital form includes a desired number of bits (N) at a predetermined sampling rate (F_s). The electrical signal, which is in the digital form, is presented to a filter 114. The filter 114 blocks the DC component of the electrical signal. The filter 114 removes low frequencies from the electrical signal. In one embodiment, the low frequencies include frequencies less than about 100 Hertz. The electrical signal with the low frequencies removed is presented as a signal 116. The signal 116 is presented to the rest of the system 100 for processing.

The signal 116 also forms a feedback signal 118. The feedback signal 118 is

presented to a detector 120. In one embodiment, the detector 120 inhibits apparent modulation in the feedback signal 118 so as to inhibit distortions in the signal 116. In another embodiment, the detector 120 forms a smooth envelope of the feedback signal 118. The smooth envelope is a filtered estimate of the feedback signal 118. The smooth envelope lacks the apparent modulation. Because of the absence of the apparent modulation in the smooth envelope, distortion of the signal 116 is inhibited.

The detector 120 presents the smooth envelope to an adjuster 122. The adjuster 122 adjusts the gain of the preamplifier 110 if the smooth envelope is above or below a threshold. The adjuster 122 adjusts the gain of the preamplifier 110 by producing an adjustment signal. In one embodiment, the adjustment signal is in a digital form. The digital form includes a desirable number of bits (M) at a predetermined sampling rate (F_s).

The adjuster presents the adjustment signal to a digital-to-analog converter 124. The digital-to-analog converter converts the adjustment signal from the digital form to an analog form. In analog form, the adjustment signal is an analog adjustment that is used by the preamplifier 110. The adjustment signal lacks the apparent modulation. The preamplifier 110 amplifies the electrical signal using the adjustment signal so as to form an amplified electrical signal. The amplified electrical signal excludes the amplitude modulation that would have formed if the adjustment signal were to include the apparent modulation. Thus, the amplified electrical signal contains desired frequency contents and lacks the amplitude modulation that gives rise to distortions.

In one embodiment, the detector 120 includes a Hilbert filter. The Hilbert filter receives the feedback signal 118 and produces two signals that are 90 degrees out of phase with each other. The detector 120 squares each signal of the two signals. The detector 120 then sums the two squared signals to form the smooth envelope. In another embodiment, the detector 120 takes the square root of the sum of the two squared signals to form the smooth envelope.

Figure 2 is a graph of an input signal according to one embodiment of the invention. The following discussion of Figure 2 is for the purpose of illustration only. The graph 200 graphs a signal that is present in a digital automatic gain control loop. This signal exists after the act of detecting the envelope but before the act of adjusting

the gain. The abscissa of the graph 200 represents time in seconds. The ordinate of the graph 200 represents amplitude of the signal.

The signal is a 5.01 kHz sine wave that has been sampled at 20 kHz. 5.01 kHz does not divide 20 kHz by exactly an integer fraction. Thus, according to the discussion hereinbefore, the signal appears as if it includes an apparent modulation. The graph 200 confirms that the amplitude of the signal appears modulated. The apparent modulation occurs as if the waveform of the electrical signal is modulated with another signal. Mathematically, this other signal appears to be a rectified sine wave with a frequency value of $n[F_s m/n - F_{\text{input}}]$. n includes a set of whole numbers that is greater than 1. F_s is the sampling frequency. m includes a set of whole numbers excluding 0. F_{input} is the frequency of the electrical signal being input into the automatic gain control.

This apparent modulation is the genesis that causes distortions when the apparent modulation is transferred to the gain during the act of adjusting the gain and eventually to the signal during the act of amplifying the signal by the preamplifier. It is this apparent modulation that is inhibited by the embodiments of the invention.

The graph 200 shows that the apparent modulation includes a depth of modulation. This depth of modulation can be used in this circumstance to understand how much distortion is present in the signal: the deeper the depth of modulation, the greater the distortion. The depth of the modulation depends on whether the frequency of the signal is evenly divisible by the sampling frequency. If it is evenly divisible, or a rational factor, the depth of modulation depends on the difference of the frequency of the signal and the nearest rational factor of the sampling frequency, the actual frequency of the signal, and the bandwidth of the control loop. The smaller the difference and the higher the signal frequency, the greater the depth of modulation, for signals within the control bandwidth.

What is shown in the graph 200 is the apparent modulation that may give rise to the amplitude modulation and hence the distortions when the signal is amplified by the preamplifier. The amplitude modulation will also include a depth of modulation. This depth of modulation tends to be greater as the level of the signal rises above the threshold of the adjuster of the digital automatic gain control.

Figures 3-4 are graphs of a signal according to one embodiment of the invention. These graphs are for the purpose of illustration only. Figure 3 shows a graph 300A of an input signal into a sound system having a digital automatic gain control. The graph 300A graphs an input signal that is presented to a digital automatic gain control. The abscissa of the graph 300A represents time in seconds. The ordinate of the graph 300A represents amplitude of the signal.

The graph 300A graphs a portion 302A of the signal that has an amplitude above the threshold of the digital automatic gain control. As discussed hereinbefore, the digital automatic gain control will reduce the amplitude of the input signal in the portion 302A by adjusting the gain of the preamplifier. A portion 304A of the graph 300A has an amplitude below the threshold of the digital automatic gain control. As discussed hereinbefore, the digital automatic gain control will increase the amplitude of the input signal in the portion 304A by adjusting the gain of the preamplifier.

Figure 4 shows a graph 300B of an output signal in a sound system having a digital automatic gain control. The graph 300B graphs an output signal that is produced by a digital automatic gain control. This output signal is processed from the input signal as shown in the graph 300A of Figure 3. The abscissa of the graph 300B represents time in seconds. The ordinate of the graph 300B represents amplitude of the signal.

A portion 302B of the graph 300B reflects the effort of the digital automatic gain control to reduce the amplitude of the input signal. The peaks of the signal in portion 302B tend to be discontinuous. These discontinuous peaks of the portion 302B are indicative of distortion in the signal. This distortion arises from the amplitude modulation of the signal that is inhibited by the embodiments of the invention. A portion 304B of the graph 300B reflects the effort of the digital automatic gain control to increase the amplitude of the input signal. The portion 304B shows a gradual increase in the amplitude over time.

Figure 5 shows a graph 400 of an output signal in a sound system having a digital automatic gain control. The graph 400 graphs an output signal that is produced by a digital automatic gain control. This output signal is processed from the input signal as shown in the graph 300A of Figure 3. The abscissa of the graph 400

represents time in seconds. The ordinate of the graph 400 represents amplitude of the signal.

A portion 402 of the graph 400 indicates that the amplitude of the input signal is successfully reduced. Note that the peaks of the output signal are parabolic and not discontinuous. This indicates that the signal lacks the distortion that is caused by the amplitude modulation as discussed hereinbefore. A portion 404 of the graph 400 shows that the amplitude of the input signal is successfully increased.

Figure 6 is a block diagram of a system according to one embodiment of the invention. A system 500 receives a signal, which represents sound energy, from a microphone 502. The signal enters a preamplifier 504. The preamplifier 504 amplifies the signal so that the signal has strength for subsequent processing by the system 500. The signal, which is amplified, enters an analog-to-digital converter 506. The analog-to-digital converter 506 converts the signal to a digital signal. The digital signal is in a form that can be easily processed by a digital integrated circuit. The digital signal enters a decimator 508. The decimator 508 reduces the number of samples while increasing the word length in the digital signal for subsequent processing of the digital signal. The digital signal, which has been decimated, enters an interpolator 512. After interpolation by the interpolator 512, the digital signal enters a digital-to-analog converter 514. The digital-to-analog converter 514 converts the digital signal to an analog signal. The analog signal enters a speaker 516. The speaker 516 reproduces sounds from the analog signal.

The digital signal, which has been decimated by the decimator 508, is also processed by a digital automatic gain control 517. Recall that the digital automatic gain control 517 helps to change the gain of the preamplifier 504. Specifically, the digital signal enters a filter 518. The filter 518 filters out low frequencies in the digital signal. In one embodiment, the low frequencies include frequencies below 100 Hertz.

The digital signal, which has been filtered, enters a detector 519. The detector 519 uses Hilbert filters to detect the envelope of the digital signal. Specifically, the digital signal enters a digital delay element 520. The digital delay element 520 delays the digital signal and produces a delayed signal. The delayed signal enters a first Hilbert filter 524. The first Hilbert filter comprises an infinite impulse response filter.

The first Hilbert filter 524 filters the delayed signal to form a first filtered signal. Besides presenting itself to the digital delay element 520, the digital signal also enters a second Hilbert filter 522. The second Hilbert filter comprises another infinite impulse response filter. The second Hilbert filter 522 filters the digital signal to form a second filtered signal.

The first filtered signal enters a first multiplier 528. The first multiplier 528 squares the first filtered signal to form a first squared signal. The second filtered signal enters a second multiplier 526. The second multiplier 526 squares the second filtered signal to form a second squared signal. Both the first squared signal and the second squared signal enter an adder 530. The adder 530 adds the first squared signal and the second squared signal together to form a sum-of-square signal.

The sum-of-square signal enters a limiter 532. The limiter 532 limits the digital range of the sum-of-square signal to a desired operating range. The sum-of-square signal then enters an adder 536. The adder 536 determines the difference between the sum-of-square signal and a threshold 534. The sum-of-square signal is an envelope of the digital signal that is produced by the detector 519. Thus, in another view, the adder 536 determines the difference between the envelope of the digital signal and a threshold 534. As will be discussed, this difference is used to adjust the gain of the preamplifier 504.

The difference determined by the adder 536 enters an adjuster 538. The adjuster 538 also receives the previous gain, an attack time constant, and a release time constant. The previous gain is the gain previously adjusted by the adjuster 538. The attack time constant is used to decrease the gain, and the release time constant is used to increase the gain.

If the difference is negative, the adjuster 538 increases the gain of the preamplifier 504. The gain is increased by shifting the bits of the previous gain to the right by the release time constant, and taking the negative of the result of the shifting. In other words, when the envelope of the digital signal is below the threshold 534, the gain of the preamplifier 504 should be increased. Such increase depends on the previous gain. The new gain is obtained by multiplying the previous gain by the inverse of a power of two. The modifier in this instance has a direct relationship to the

release time constant. The discussed implementation uses shifts, which is equivalent to multiplications by inverse powers of two, to implement the time constants, but it should be understood that these time constants can be implemented by other techniques, such as by regular multiplies.

5 If the difference is positive, the adjuster 538 decreases the gain of the preamplifier 504. The gain is decreased by shifting the bits of the difference to the right by the attack time constant. In other words, when the envelope of the digital signal is above the threshold 534, the gain of the preamplifier 504 should be decreased. Such decrease depends on the difference between the envelope of the digital signal and the
10 threshold. The new gain is obtained by multiplying the difference by the inverse of a power of two. The modifier in this instance has a direct relationship to the attack time constant.

 The new gain enters an adder 540. The adder 540 adds the new gain to an adjusted previous gain to form the gain. The adjusted previous gain is formed from a
15 width adjuster 542 that adjusts the width of the word of the previous gain. The gain enters a limiter 544. The limiter 544 limits the range of the gain. The gain then enters a buffer 546. The buffer 546 stores the gain and presents the gain to a rounding circuit 548. The buffer 546 also feeds back the gain to the width adjuster 542 and the adjuster 538. The rounding circuit 548 rounds the gain to a smaller precision value so as to be
20 compatible with the input width of subsequent circuitry.

 The gain, which is rounded, enters a digital-to-analog converter 550. The digital-to-analog converter 550 converts the gain from digital to analog and presents the gain, which is now analog, to the preamplifier 504. The preamplifier 504 uses the gain to amplify the signal, which represents sound energy, from the microphone 502.

25 Figure 7 is a block diagram of a filter according to one embodiment of the invention. The filter 600 acts to filter out low frequencies from a digital signal. The digital signal enters both a first adder 604 and a first digital delay element 602. The first digital delay element 602 delays the digital signal to produce a delayed digital signal. The adder 604 determines the difference between the digital signal and the
30 delayed digital signal. This difference enters a multiplier 606. The multiplier 606 multiplies the difference by a scale 608 to produce a scaled signal. The scale 608 is

used to inhibit the filter 600 from overflow. The scaled signal enters a second adder 610. The second adder 610 adds the scaled signal with a block signal to produce a filtered signal. The block signal will be discussed hereinafter. The filtered signal enters a second digital delay element 616. The second digital delay element 616 delays the filtered signal. The filtered signal then exits the filter 600. A portion of the filtered signal feeds back into a second multiplier 614. The second multiplier 614 multiplies the filtered signal, which is delayed, by an alpha signal to form the blocked signal. The alpha signal determines a range of frequencies that will be blocked by the filter 600.

Figure 8 is a block diagram of a filter according to one embodiment of the invention. A filter 700 is an infinite-impulse response filter. The filter 700 is configured as a two-zeros two-poles filter. The filter 700 can be used as a Hilbert filter in a detector as part of a digital automatic gain control circuit. The digital signal enters a first digital delay element 702, a second digital delay element 704, and a scale element 712. Thus, the digital signal is delayed by the first digital delay element 702, delayed by the second digital delay element 704, and scaled by the scale element 712 to produce a scaled signal.

The digital signal also enters a first adder 706. The first adder 706 determines the difference between the digital signal and the feedback signal. The difference enters a multiplier 708. The multiplier 708 multiplies the difference and a beta signal 710 to form a modified signal. The beta signal 710 acts to control the phase of the difference. The beta signal contains a number of bits that is used to represent a desired number to be input into the multiplier 708.

The modified signal enters a third digital delay element 716. The third digital delay element 716 delays the modified signal to form a filtered signal. The filtered signal exits the filter 700 to be used by other circuitry. A portion of the filtered signal enters a fourth digital delay element 718. The fourth digital delay element 718 delays the filtered signal to form the feedback signal.

Figure 9 is a process diagram of a method according to one embodiment of the invention. The process 800 discusses the feedback loop that analyzes the digital signal and determines whether the level of the digital should be adjusted. The process 800 begins at an act 802. The act 802 converts an analog signal to a digital signal. The

digital signal is presented to an act 804. The act 804 blocks low frequencies from the digital signal to produce a filtered signal. In one embodiment, the low frequencies, which are blocked, are less than about 100 Hertz.

5 The filtered signal is presented to an act 806. The act 806 forms an envelope that lacks the apparent modulation. One suitable technique of forming an envelope that lacks the apparent modulation includes using Hilbert filters. The envelope is presented to an act 810. The act 810 subtracts the envelope from a threshold to form a difference. The difference is presented to acts 812 and 814.

10 The act 812 determines if the difference is greater than zero. If the difference is greater than zero, the gain should be decreased. In other words, the envelope of the digital signal is greater than the threshold. The digital signal is at a level beyond the operating range of a processing system and such level should be decreased. If the difference is less than zero, then the gain should be increased. When the envelope of the digital signal is less than the threshold, the digital signal should be strengthened by
15 increasing the gain for subsequent processing.

The result of the act 812 is presented to an act 818. The act 818 uses the result of the act 812 to select the result of either act 814 or act 816 to form a gain. Thus, the act 818 switches between the result of the act 814 or the act 816 depending on the result of the act 812. If the gain needs to be decreased, the act 818 selects the result of the act
20 814. The act 814 decreases the gain by shifting the bits of the difference to the right by an attack constant. If the gain needs to be increased, the act 818 selects the result of the act 816. The act 816 increases the gain by shifting the bits of the feedback signal, which is delayed and negated, to the right by a release constant.

The gain, which is formed by the act 818, is presented to an act 824. The act
25 824 sums the gain and the feedback signal, which is delayed. The feedback signal, which is delayed, is formed by an act 822. The act 820 negates the feedback signal, which is delayed, and presents the result to the act 816 as discussed hereinbefore.

The act 826 equates the gain to 0 if the gain is less than or equal to zero. Otherwise, the act 828 equates the gain to 1 if the gain is greater than 1. The result of
30 the act 826 and the act 828 is presented to an act 830. The act 830 converts the digital form of the gain to an analog form, which is suitable for an analog preamplifier.

Figure 10 is a diagram of a signal processing system 1000 according to the teachings of the present invention. System 1000 includes the digital automatic gain control system 100 as described herein and a signal reconstruction system 1001. In an embodiment, signal reconstruction system 1001 includes a feed forward digital circuit.

5 Signal reconstruction system 1001 includes a transfer function element 1005 that receives the digital amplifier control signal 1004 from the loop control 122. Signal 1004 includes a digital form that has a desirable number of bits (M) at a predetermined sampling rate (F_s). The transfer function element 1005 produces a compression recapture signal 1007 based on the amplifier control signal 1004. Signal 1007 includes
10 a digital form that has a desirable number of bits (J) at a predetermined sampling rate (F_s). In an embodiment, the compression recapture signal 1007 is fed to a signal processor. Thus, the compression recapture or restoration circuit is a feed forward circuit whereas the automatic gain control circuit is a feed back circuit.

In an embodiment, the system 1000 includes a multiplier 1010. Multiplier 1010
15 receives digital output signal 116 from digital automatic gain control system 100 and compression recapture signal 1007 from transfer function element 1005. Multiplier 1010 combines digital compression recapture signal 1007 and digital output signal 116 to produce a digital signal 1020 that is fed to the digital signal processor. Signal 1020 includes a digital form that has a number of bits (N+J) at the predetermined
20 sampling rate (F_s).

In operation, system 1000 provides the required input signal compression to keep the input stage elements in a linear operating range while not losing the information in the compressed portion of the input signal. This is achieved by using the variable gain control signal 1004 to both control the variable gain and restore the
25 compressed part of the input signal. In an embodiment, restoration is accomplished digitally.

More specifically, loop control 122 produces a digital signal 1004 that causes the variable gain amplifier 110 to compress the analog input signal. As described herein, the input signal is compressed to keep to the analog to digital converter 112 in
30 its linear operating range. The digital signal 1004 is linearly related to the change in gain in the variable amplifier 110. A first example of signal 1004 is a first signal that

represents reducing the gain of amplifier 110 to half the first signal's original amplitude. The first signal 1004 is produced by the automatic gain control circuit 100 based on an input signal. A second example of signal 1004 is a second signal that represents reducing the gain of amplifier 110 by a factor of ten. The transfer function element 1005 inverts the variable gain control signal 1004 to produce the compression recapture signal 1007. In the first example, compression recapture signal 1007 is a signal that represents doubling the output signal 116 to produce output signal 1020. In the second example, compression recapture signal 1007 is a signal that represents increasing the output signal 116 by a factor of ten to produce output signal 1020.

In the field of hearing aids it is desirable to make the relationship between the feedback signal 1004 to be linearly related to the gain of the amplifier 110. Some of the variables that would be controlled to achieve the linear relationship include the digital word width of signal 1004 and the precision of the relationship between the actual amplifier gain and the digital signal 1004.

In an embodiment of the invention, the transfer function element 1005 includes a lookup table or mapping device. Such an element 1005 takes the control signal 1004 and correlates it to a corresponding compression recapture signal 1007. The corresponding signal 1007 is sent to the digital signal processor or combined with the AGC system output signal 116 to form signal 1020. Signal 1020 now digitally represents the analog input signal before it was compressed. This embodiment is used when the signal 1004 represents the required gain reduction which is converted to an analog signal by DAC 124. The analog signal controls the variable gain of amplifier 110.

The open loop nature of the feed-forward signal reconstruction system 1001 requires a close match to the transfer characteristics of the digital automatic gain control system 100. Accordingly, the automatic gain control system 100 must have stable transfer characteristics. Factors that must be considered are operating environment, e.g., temperature, and manufacturing variations. Stable transfer characteristics in system 100 will allow its transfer characteristics to be accurately matched, ideally 1:1, to the transfer characteristics of signal reconstruction system 1001. The use of a digital AGC system 100 provides the required control of tolerances and variations in the circuit

and thus provides stable signal transfer characteristics.

Signal reconstruction system 1001, in an embodiment, includes structures and methods for reducing sampling effects. The sampling effects may include first-order sampling effects.

5 Figures 11-15 show the performance of system 1000 when it receives a signal as shown in Figure 11. Figure 11 include a graph 1100 of the output signal versus the input signal of microphone 102. Note that the graph assumes ideal performance of the microphone 102.

10 Figure 12 shows a graph 1200 of signal and noise characteristics at the analog to digital convertor 122 in a sound system having digital automatic gain control and digital compression recapture. Graph 1200 graphs an output signal that is produced by a digital automatic gain control. The output signal graph 1200 includes a first portion 1201 that reflects a linear relationship between the input (abscissa) and the output (ordinate). The output signal graph 1200 further includes a compressed, second portion 15 1202. In this example, the input signal is compressed above 90dB, which results in the output signal being flat (i.e., constant at 90dB) for any input signal above 90dB. The compression of the signal is accomplished according to the methods and structures as explained herein at threshold of 90dB.

20 Figure 13 shows a graph 1300 of signal at the transfer function element 1005 in a sound system having digital compression recapture. Graph 1300 graphs an output signal that is produced by a compression recapture system 1001. When the input signal to the system 100 remains at or below a threshold value, then the AGC system does not provide a gain to reduce the amplitude of the input signal. The compression recapture system 1001 does not produce an output signal 1007 because a gain is not applied to 25 compress the input signal. That is, signal 1007 is at zero dB when the input signal is below the threshold value. In the illustrated embodiment, the threshold value is 90dB, however, other embodiments of the present invention are not limited to a 90dB threshold value. The output signal graph 1300 is a recoded signal that represents the compressed portion of input signal 1100. The compressed portion of input signal 1100 30 is determined by the element 1005 based on the digital gain control signal 1004. In present embodiment, graph 1300 represents the portion of the input signal above the

90dB threshold. In an embodiment, graph 1300 is the mathematical inverse of the gain applied to compress the input signal. Thus, multiplying the output signal shown at 1300 with the signal 116 rebuilds the digital signal to essentially match the input signal.

Figure 14 shows a graph 1400 of signal and noise characteristics at the processor in a sound system having digital automatic gain control and digital compression recapture according to the teachings of the present invention. The input of graph 1400 is the digital signal 1020 which includes the compressed signal 116 from gain control input system 100 and the recaptured compressed signal 1007 from the signal reconstruction circuit or system 1001. Graph 1400 digitally represents the output signal from microphone 102 as shown in Figure 11 including the compressed portion 1202. Graph 1405 represents the signal 116 without the compression recapture, which would be provided to the digital signal processor.

Figure 15 shows a graph 1500 of an output signal in a sound system having digital automatic gain control and digital compression recapture. The graph 1500 graphs an output signal that is produced by a digital automatic gain control with digital compression recapture. This output signal is processed from the input signal as shown in the graph 300A of Figure 3. The abscissa of the graph 1500 represents time in seconds. The ordinate of the graph 1500 represents amplitude of the signal.

A portion 1502 of the graph 1500 indicates that the amplitude of the input signal is successfully reduced and output as signal 116 (Figure 10). Note that the peaks of the output signal are parabolic and not discontinuous. This indicates that the signal lacks the distortion that is caused by the amplitude modulation as discussed hereinbefore. A portion 1504 of the graph 1500 shows that the amplitude of the input signal is successfully increased according to the teachings herein.

Graph 1500 further indicates that the compressed portion of the input signal is added to signal portions 1502 and 1504 to produce signal 1505. Signal 1505 is a essentially rebuilt version of input signal 302A. That is, compression recapture system 1001 reinserts the compressed portion 1507 of the input signal back into the processed signal prior to sending it to the processor. More specifically, the compression recapture system 1001 reverses the compression applied to the input signal. Thus, the amplitude information of input signal 302A above the threshold level is not discarded and is added

back into the digital signal 1020 output from input stage or system 1000. Accordingly, the digital signal processor receives a signal that includes the compressed portion.

An embodiment of the present invention includes manufacturing the system 1000 in a single integrated circuit. Such integration will save on size and power consumption while increasing the front end transducing range. Size and power are valuable commodities in hearing aid applications.

The present invention improves the transducing range of the input stage 1000. Transducing range for input stage 1000 is defined as the range from the smallest input signal that can be accurately transduced through the input stage 1000 to the largest signal that can be accurately transduced through the input stage 1000. Input stage 1000 has a transducing range that extends above the threshold value by using the recapture system 1001. For example, the transducing range of the input stage producing the signals in Figures 11-14 is 90dB (smallest input above noise floor equals 20 dB, largest signal input equals 110dB). While the illustrated example shows the largest input signal as 110dB, the present invention is not so limited. The 110dB input signal represents an upper limit of a microphone. By using the compression recapture system 1001, it is believed that the upper input limit is essentially unlimited if adequate precision and word width are available in the digital automatic gain control and digital recapture signals. Accordingly, the present invention provides faithful transducing of an input signal above the noise floor. Moreover, the transducing of the signal using the present invention provides linear transducing above the noise floor and above the linear range threshold values for components in the input stage. The present invention has linear transducing of an analog input signal to a digital representation of that analog signal as an output signal.

Conclusion

Thus, systems, devices, and methods have been discussed for inhibiting undesired amplitude modulation which causes distortions in the amplified signal in a sound system. The embodiments of the invention inhibit such undesired amplitude modulation by reducing apparent sampling rate distortion.

The digital system as described has a number of benefits not seen before. One

benefit is an enhanced manufacturing process that reduces a need for external components, such as capacitors, and the need to couple the external components to a circuit through I/O pins. Another benefit includes a reduction in the die area required to implement the digital automatic gain control loop. Other benefits include an enhanced
5 control of the tolerance of the bandwidth of the automatic gain control, and the tolerance of the loop time constants of the automatic gain control. The system also benefits from an enhanced power efficiency and low operating voltage performance. Additionally, the system allows a non-linear signal processing by selectively controlling the gain of the preamplifier or providing information to a Nicest-rate digital signal
10 processor to compensate for adaptive gain changes in the preamplifier.

The digital system as described includes further benefits of reconstructing an input signal that has been compressed by a preamplifier. The digital system uses the digital variable amplifier control signal to reconstruct the input signal to include the compressed portion. Thus, the input signal can be reconstructed digitally and fed to a
15 digital signal processor. In a hearing aid application of the present invention, the compressed amplitude of the sound signal is reconstructed. Thus, amplitude information in the sound signal that was compressed is recaptures. The transducing range of the hearing aid is accordingly enhanced. Moreover, such an enhancement of the transducing range results in more information in the signal that is passed to the
20 signal processor and to the hearing aid wearer. Further, the increase in transducing range is within the limitations of front end noise for hearing aid applications, does not increase component sizes, and does not require an increased voltage. Moreover, restoring the amplitude information in the signal may restore information into the signal, which may be important information to a hearing aid wearer. The present
25 invention reverses the effects of non-linear application of gain and compression to reconstruct the original (prior to compression) signal based on the information used to compress the signal.

Although the specific embodiments have been illustrated and described herein, it will be appreciated by those of ordinary skill in the art that any arrangement which is
30 calculated to achieve the same purpose may be substituted for the specific embodiment shown. This application is intended to cover any adaptations or variations of the

present invention. It is to be understood that the above description is intended to be illustrative and not restrictive. Combinations of the above embodiments and other embodiments will be apparent to those of skill in the art upon reviewing the above description. The scope of the invention includes any other applications in which the
5 above structures and fabrication methods are used. Accordingly, the scope of the invention should only be determined with reference to the appended claims, along with the full scope of equivalents to which such claims are entitled.